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BORESIGHT SLOPE OPTIMIZATION OF SUB-ARRAYED LINEAR  
ARRAYS THROUGH THE CONTIGUOUS PARTITION METHOD

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# Boresight Slope Optimization of Sub-arrayed Linear Arrays through the Contiguous Partition Method

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## Abstract

The optimization of the normalized boresight slope of the difference pattern in sub-arrayed linear monopulse antennas is presented. The knowledge of the independently optimum difference excitations, which provide the maximum normalized boresight slope, is exploited with an efficient excitation matching technique based on the contiguous partition method. A set of numerical experiments are provided to assess the effectiveness of the proposed method in reaching the best achievable performances even though with a small number of sub-arrays.

## Index Terms

Monopulse array antennas, Sum and difference patterns, Boresight slope.

## I. INTRODUCTION

In the framework of radar applications, a key feature of the antenna systems is the ability to afford a difference pattern with a null as deep as possible in the boresight direction [1]. As a matter of fact, such a characteristic determines the sensitivity of the radar in term of angle resolution. In [2], it has been shown how to obtain the maximum angular sensitivity (i.e., the deepest slope on boresight) in the case of a linear odd amplitude distribution. As regards to monopulse radar [3], Baylis distributions are usually used since they allow the synthesis of patterns with a good trade-off between low-sidelobe and narrow beamwidth. Unfortunately, the synthesized patterns do not present the maximum normalized slope for a given array geometry. Moreover, a complete and dedicated feed network would be required to generate such a difference mode [3][4]. The use of two independent feed networks for the sum and difference patterns is often unacceptable, because of the complexity of the *HW* realization and the arising costs. In order to overcome these drawbacks, several techniques, which share parts of the feed network to generate the sum and the difference patterns, have been presented in the literature [5]-[10]. More in detail, one set of excitations (either the sum or the difference coefficients) is *a-priori* fixed to afford an optimum pattern. The other pattern is obtained by properly grouping the array elements into sub-arrays and assigning to each sub-array a suitable gain to match some constraints on the generated beam.

As far as the literature on such a topic is concerned, the approximation of a reference pattern has been considered in [5][10], wherein the “best compromise” has been computed by means of excitation matching procedures. On the other hand, in [6]-[9] the optimization of the sidelobe level (*SLL*) of the difference pattern, for a pre-fixed sum mode, has been considered.

The optimization of other pattern features has been faced in [11] and in [9] where the directivity and the slope on the boresight, together with a proper control of the *SLL*, of the difference pattern have been optimized through a differential evolution (*DE*) method and a hybrid approach, respectively. In this letter, the contiguous partition method (*CPM*) [10] is applied to the optimization of the boresight slope of the difference pattern. In particular, since the *CPM* has shown its effectiveness not only in synthesizing a difference pattern close as much as possible to the optimum one in the Dolph-Chebyshev sense [10], but also in minimizing the *SLL* [12] of difference beams, this work is aimed at showing its potentialities and limitations as well as its flexibility also in this context. Moreover, a comparison with the results in [9] is also reported to shown how the proposed approach compares with others in the literature.

The paper is organized as follows. In Sect. 2, the problem is mathematically formulated by detailing the synthesis procedure. In Sect. 3, selected results are reported to assess the validity and versatility of the *CPM*-based technique. Finally, some conclusions are drawn (Sect. 4).

## II. MATHEMATICAL FORMULATION

Let us consider a linear array of  $M = 2 \times N$  elements uniformly-spaced of  $d$ . Following the monopulse principle, the sum pattern is given by the set  $\alpha_n$ ,  $n = \pm 1, \dots, \pm N$  of symmetric excitations ( $\alpha_n = \alpha_{-n}$ ), while anti-symmetric coefficients ( $\beta_n = -\beta_{-n}$ ) generate on receive the difference beam. Accordingly, sum and difference patterns are obtained by adding and subtracting the two halves of the antenna aperture [13].

When a sub-arraying technique is adopted to generate the difference mode from the sum one [5], the synthesis problem is recast as the definition of a suitable grouping, described through the integer indexes  $c_n \in [1 : Q]$ ,  $n = 1, \dots, N$ , and the sub-array gains  $w_q$ ,  $q = 1, \dots, Q$ , to fit some user-defined requirements. In particular, the compromise difference pattern is obtained from the coefficient set

$$\underline{B} = \{b_n = -b_{-n} = \alpha_n \delta_{nq} w_q; n \in [1 : N]; q \in [1 : Q]\}. \quad (1)$$

where  $\delta_{nq}$  is the Kronecker delta equal to  $\delta_{nq} = 1$  if  $c_n = q$  and  $\delta_{nq} = 0$  otherwise.

Since the problem at hand is concerned with the maximization of the boresight slope of the difference pattern and the *CPM* is an excitation matching approach aimed at fitting a reference pattern, it is needed to determine the optimal pattern in terms of slope. Concerning the metric to be used to quantify the boresight slope of an array of discrete elements, the *difference slope ratio* is considered [14]. It is defined as  $K_r = \frac{K}{K_0}$ ,  $K$  and  $K_0$  being the normalized boresight slope of the actual difference beam and the maximum value that would be achieved with a line source distribution on the antenna aperture of size  $L/\lambda$ , respectively. In the linear case, it has been shown in [2] that the distribution providing the maximum value of  $K_0$  is a linear odd (with respect to the center of the antenna aperture) distribution. Accordingly, since  $K_0$  is known once the array geometry is given, the synthesis procedure for a discrete element array is aimed at maximizing the value of the normalized boresight slope  $K$ . Such a value for an anti-symmetric set of excitations is given by [14]

$$K = \frac{\sum_{n=1}^N \{k_n \beta_n\}}{\sqrt{2 \sum_{n=1}^N \sum_{m=1}^N \{\beta_n G_{nm} \beta_m\}}} \quad (2)$$

where  $k_n = \frac{2n-1}{2N-1}$  and  $G_{nm} = \frac{\sin[(m-n)kd]}{(m-n)kd} - \frac{\sin[(m+n-1)kd]}{(m+n-1)kd}$ . Accordingly, the first step of the compromise synthesis procedure is aimed at computing the excitation coefficients  $\underline{B}^{opt} = \{b_n^{opt}; n = \pm 1, \dots, \pm N\}$  that afford a pattern with the maximum normalized boresight slope  $K_{max}$  in the case of discrete element arrays. Towards this end, the functional (2) is maximized by means of a standard steepest-descent method according to the procedure described in [14]. Afterward, the *CPM* is exploited to find the ‘‘best compromise’’ between sum and difference patterns such that the excitations  $\underline{B}$  be close as much as possible to the reference ones  $\underline{B}^{opt}$ . In particular, once the sum mode coefficients  $\alpha_n$ ,  $n = 1, \dots, N$  are fixed to provide an optimum sum pattern (e.g., a Taylor pattern [15]), the following cost function

$$\Psi(c_n, w_q) = \frac{1}{N} \left\{ \sum_{n=1}^N |g_{nq}|^2 \right\} \quad (3)$$

where  $g_{nq} = \alpha_n \left[ \gamma_n - \sum_{q=1}^Q \delta_{nq} w_q(c_n) \right]$  and  $\gamma_n = \frac{b_n^{opt}}{\alpha_n}$ , is minimized with respect to the unknowns  $(c_n, w_q)$ ,  $n = 1, \dots, N$ ;  $q = 1, \dots, Q$ .

It is worth to notice that, equation (3) mathematically formalizes a minimum variance problem, where each term is related to a different sub-array. Since the value minimizing the sum of the square distances, for a given set of real values, is the weighted arithmetic mean, the sub-array weights turn out to be

$$w_q(c_n) = \frac{\sum_{n=1}^N (\alpha_n)^2 \delta_{nq} \gamma_n}{\sum_{n=1}^N (\alpha_n)^2 \delta_{nq}}, \quad q = 1, \dots, Q. \quad (4)$$

As a consequence, the problem solution recast as the definition of only the sub-array aggregations  $c_n$ ,  $n = 1, \dots, N$ . With reference to (3), let us observe that such a solution is a least square partition and Fisher in [16] proved that it is a *contiguous*

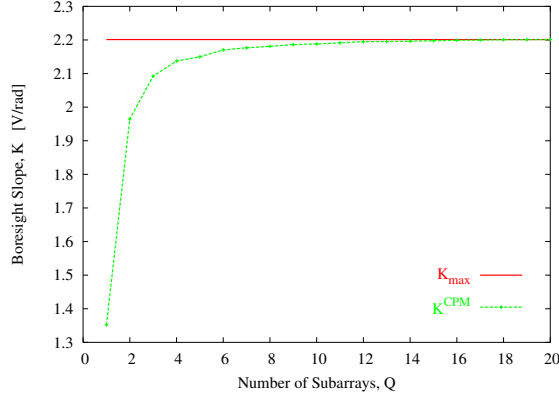


Fig. 1. *Test Case 1* ( $N = 20$ ,  $d = 0.7\lambda$ , *Taylor sum pattern* [15] -  $SLL = -30$  dB,  $\bar{n} = 6$ ) - Value of the normalized boresight slope versus the number of sub-arrays  $Q$ .

*partition*<sup>1</sup> ( $CP$ ) of the ordered list of the *optimal gains*  $\gamma_n$ . Since the number of  $CP$ s is equal to  $U = \binom{N-1}{Q-1}$ , the dimension of the solution space of the  $CPM$  considerably reduces compared to that of classical optimization-based approaches [6]-[9]. In order to sample such a space, the *Border Element Method* ( $BEM$ ) [10] is used. Starting from a randomly chosen contiguous partition  $\underline{C}^{(0)} = \{c_n^{(0)}; n = 1, \dots, N\}$ , the trial solution is updated,  $\underline{C}^{(i)} \leftarrow \underline{C}^{(i+1)}$ , taking into account that the *border elements* (i.e., those elements whose adjacent values  $\gamma_{n-1}$  or/and  $\gamma_{n+1}$  are assigned to a different sub-array) can change the sub-array membership without violating the condition of contiguous partition. The process is iterated until the termination criterion, based on the maximum number of iterations  $I$  (i.e.,  $i > I$ ) or on the stationariness of the cost function value (i.e.,  $\frac{|K_{\Psi} \Psi^{(i-1)} - \sum_{j=1}^{K_{\Psi}} \Psi^{(j)}|}{\Psi^{(i)}} \leq \eta_{\Psi}$ , being  $K_{\Psi}$  and  $\eta_{\Psi}$  two user-defined control parameters), is verified.

### III. NUMERICAL RESULTS

In the first example, an array of  $M = 40$  elements spaced by  $d = 0.7\lambda$  is considered. The sum pattern has been fixed to a Taylor pattern with  $SLL = -30$  dB and  $\bar{n} = 6$ . The reference difference pattern  $\underline{B}^{opt}$ , which guarantees the maximum boresight slope ( $K_{max} = 2.2013$ ) has been computed [14]. Concerning the compromise solution, the number of sub-arrays used in the non-complete feed network has been varied in the range  $Q \in [1, 20]$ . As far as the initialization of the  $BEM$  is concerned, the initial aggregation  $\underline{C}^{(0)}$  has been chosen with the array elements uniformly distributed among the  $Q$  sub-arrays. The values of  $K$  in correspondence with the solutions obtained by the  $CPM$  are shown in Fig. 1. By quantifying the closeness of the synthesized normalized difference slope on boresight to the optimal value  $K_{max} = 2.2013$  with the index  $\xi_K \triangleq \frac{K_{max} - K^{CPM}}{K_{max}} \times 100$ , it turns out that  $\xi_K \leq 3$  when  $Q \geq 4$  and  $\xi_K \leq 1$  for  $Q \geq 8$ . On the other hand, the simplification of the network architecture when  $\frac{N}{Q} \Big|_{Q=3} \simeq 7$  and  $\frac{N}{Q} \Big|_{Q=2} = 10$  causes a strong reduction of the performance (i.e.,  $\xi_K \Big|_{Q=3} = 4.95$  and  $\xi_K \Big|_{Q=2} = 10.74$ ).

The effectiveness of the  $CPM$  in sampling the solution space is pointed out by the values in Tab. I,  $I_{end}$  and  $T$  being the number of cost function evaluations to get the final solution and the total  $CPU$ -time (on a 3.4 GHz PC with 2 GB of RAM), respectively. As a matter of fact, starting from an uniform clustering ( $i = 0$ ), the trial solution is closer to the reference one just increasing the number of sub-arrays ( $\Psi^{(i)} \Big|_{Q=3} \simeq 2.9 \times 10^{-2}$ ,  $\Psi^{(i)} \Big|_{Q=5} \simeq 1.2 \times 10^{-2}$ ,  $\Psi^{(i)} \Big|_{Q=10} \simeq 2.8 \times 10^{-3}$ , and  $\Psi^{(i)} \Big|_{Q=15} \simeq 8.2 \times 10^{-4}$ ). Moreover, it should be observed that at most 40 iterations are enough to reach the convergence solutions whose excitations and corresponding patterns are shown in Fig. 2.

The second example deals with a linear array of  $N = 20$  equally-spaced ( $d = 0.5\lambda$ ) elements. The sum excitations have been set to those of the Dolph-Chebyshev pattern with  $SLL = -20$  dB [17]. Regarding the definition of the reference set of excitations  $\underline{B}^{opt}$ , it has been observed [14] that the element coefficients, for the half-wavelength spacing case, are simply computed by sampling the continuous line-source distribution in [2] (Fig. 3 - McNamara, 1987). Thus, the maximum value

<sup>1</sup> A grouping of array elements is a *contiguous partition* when given two elements  $\gamma_i$  and  $\gamma_n$  which belong to the  $q$ -th sub-array, if another element exists such that the condition  $\gamma_i < \gamma_j < \gamma_n$  holds true, hence  $\gamma_j$  has to be assigned to the same sub-array.

TABLE I

Test Case 1 ( $N = 20$ ,  $d = 0.7\lambda$ , Taylor sum pattern [15] -  $SLL = -30$  dB,  $\bar{n} = 6$ ) - COMPUTATIONAL INDEXES.

	$U$	$I_{end}$	$T$ [sec]
$Q = 3$	741	3	$3.0 \times 10^{-8}$
$Q = 5$	82251	31	$3.1 \times 10^{-7}$
$Q = 10$	$211 \times 10^6$	33	$3.3 \times 10^{-7}$
$Q = 15$	$1.50 \times 10^{10}$	9	$9.0 \times 10^{-8}$

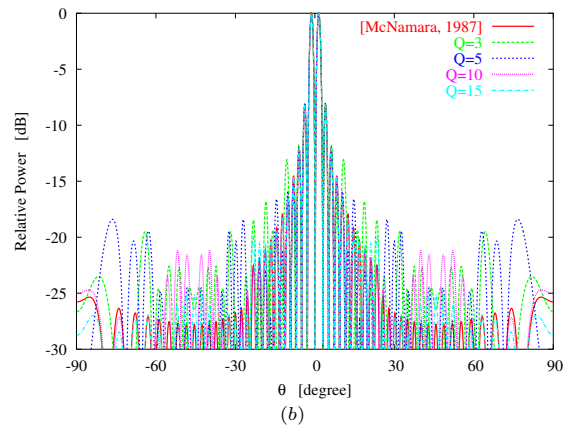
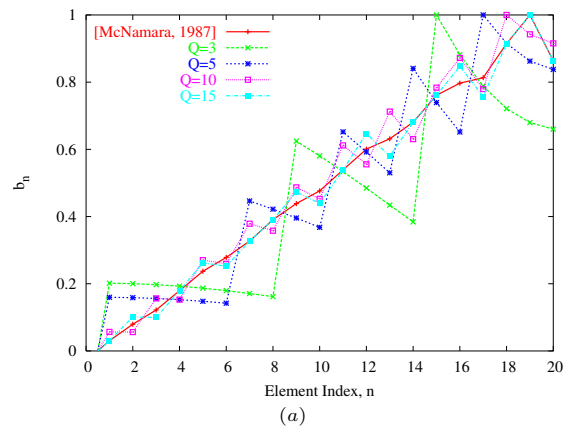


Fig. 2. Test Case 1 ( $N = 20$ ,  $d = 0.7\lambda$ , Taylor sum pattern [15] -  $SLL = -30$  dB,  $\bar{n} = 6$ ) - Plots of the (a) excitation coefficients and of the (b) corresponding relative power pattern for various values of  $Q$ .

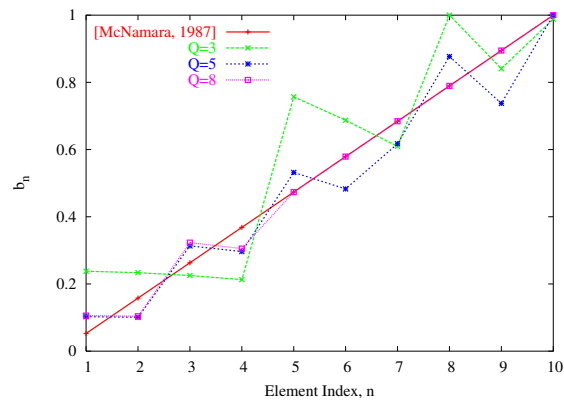


Fig. 3. Test Case 2 ( $N = 10$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - Plot of the values of the excitation coefficients for various values of  $Q$ .

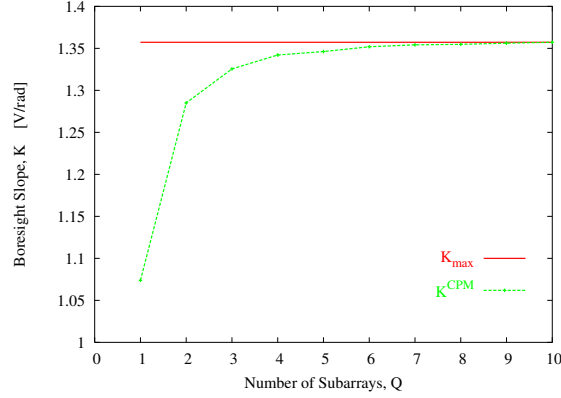


Fig. 4. *Test Case 2* ( $N = 10$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - Plot of the normalized boresight slope values versus the number of sub-arrays  $Q$ .

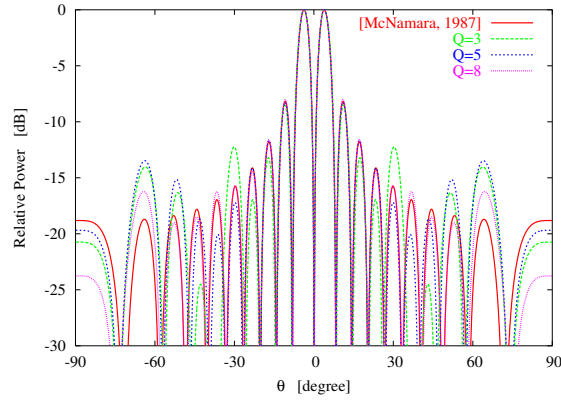


Fig. 5. *Test Case 2* ( $N = 10$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - Plot of the relative power pattern for different values of  $Q$ .

of the boresight slope for an aperture of length  $L/\lambda = 10$  is  $K_{max} = 1.3572$  [14]. Also in this case, the estimated values of  $K$  are close ( $\xi_K < 1$ ) to the reference one when  $Q > 4$  (Fig. 4). Such a circumstance is further pointed out in Fig. 3 where the synthesized coefficients get closer and closer to the reference set  $\underline{B}^{opt}$  when  $Q \rightarrow N$ .

For completeness, the difference patterns for the experiment considered in Fig. 3 are reported in Fig. 5. Moreover, the sub-array configurations and the corresponding gains are summarized in Tab. II. As far as the computational issues are concerned, the dimensions of the solution spaces are equal to  $U|_{Q=3} = U|_{Q=8} = 36$  and  $U|_{Q=5} = 126$ . Furthermore, the numbers of iterations to reach the convergence solutions are  $I_{end}|_{Q=3} = 4$ ,  $I_{end}|_{Q=5} = 1$ , and  $I_{end}|_{Q=8} = 3$ . As a result, the *CPU*-time for the synthesis is lower than  $10^{-6}$  sec.

Finally, let us compare with the result reported in [9] where the constrained (sidelobe-wise) optimization of the boresight slope is considered when  $N = 10$  and  $Q = 8$ . Towards this end, the sub-array weights are now computed solving a Convex Programming (*CP*) problem as in [9] starting from the sub-array configuration obtained by means of the *CPM*. Figure 6 shows

TABLE II

*Test Case 2* ( $N = 10$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - SUB-ARRAY CONFIGURATIONS AND SUB-ARRAY GAINS.

$c_n$	$w_q$
1 1 1 1 2 2 2 3 3 2	0.2328, 0.8925, 1.6912
1 1 2 2 3 3 4 5 5 4	0.1145, 0.3696, 0.7152, 1.0299, 1.6912
1 1 2 2 3 4 6 7 8 5	0.1145, 0.3696, 0.6184, 0.8325, 1.0, 1.1087, 1.4783, 1.9923

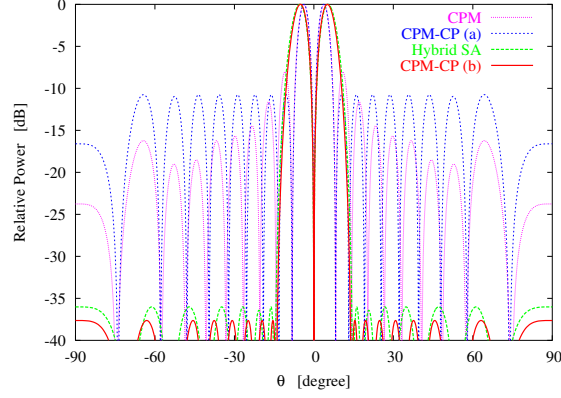


Fig. 6. *Test Case 3* ( $N = 10$ ,  $Q = 8$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - Plot of the relative power pattern obtained by the herein proposed hybrid method and that of [9].

TABLE III

*Test Case 3* ( $N = 10$ ,  $Q = 8$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - PERFORMANCE INDEXES.

	$K$ [V/rad]	$SLL$ [dB]	$BW$ [degree]
<i>CPM</i>	1.35	-8.0	3.95
<i>CPM - CP (a)</i>	1.28	-10.8	3.90
<i>Hybrid SA</i>	0.90	-35.7	5.90
<i>CPM - CP (b)</i>	0.97	-37.5	5.60

the results of the hybrid approach (*CPM - CP*, [18]) as well as those synthesized by the *CPM* and in [9]. With reference to the configuration in Tab. II, the  $SLL$  of the solution computed through the hybrid method [*CPM - CP (a)*] is almost 3 dB below that with the *CPM*, but the slope at boresight slightly worsen. Successively, more stringent constraints on the  $SLL$  are imposed to fairly compare with the solution of the *Hybrid SA* in [9]. Accordingly, a new reference pattern has been assumed (namely a Zolotarev pattern with  $SLL = -39$  dB [4]), which presents a high value of the boresight slope for a given  $SLL$ . In this case, the synthesized aggregation is  $\{c_n\} = \{1\ 2\ 3\ 4\ 4\ 4\ 5\ 6\ 7\ 8\}$ . The corresponding solution [*CPM - CP (b)*] outperforms that in [9] for both the boresight slope, the beamwidth ( $BW$ ), and the  $SLL$  (Tab. III).

Similar conclusions hold true for the case also dealt with in [9] with  $Q = 6$ , thus confirming the effectiveness and versatility of the *CPM*-based approach. In particular, Figure 7 and Tab. IV report the radiation patterns obtained with the bare *CPM* as well as the hybrid approaches (i.e., *CPM - CP* and *Hybrid SA* [9]) and their performance, respectively.

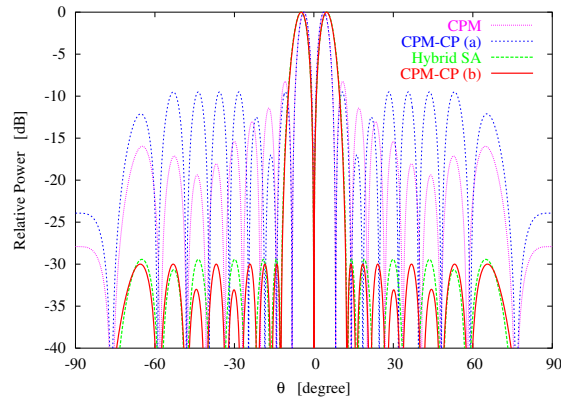


Fig. 7. *Test Case 4* ( $N = 10$ ,  $Q = 6$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - Plot of the relative power pattern obtained by the herein proposed hybrid method and that of [9].



TABLE IV

Test Case 4 ( $N = 10$ ,  $Q = 6$ ,  $d = \lambda/2$ , Dolph-Chebyshev sum pattern [17] -  $SLL = -20$  dB) - PERFORMANCE INDEXES.

	$K$ [V/rad]	$SLL$ [dB]	$BW$ [degree]
<i>CPM</i>	1.35	-8.2	3.94
<i>CPM - CP (a)</i>	1.25	-9.5	3.92
<i>Hybrid SA</i>	1.05	-29.5	5.26
<i>CPM - CP (b)</i>	1.06	-30.0	5.21

#### IV. CONCLUSIONS

In this paper, the optimization of the normalized boresight slope of the difference pattern of monopulse array antennas has been carried out by means of the *CPM*. In particular, the sub-arraying configuration has been taken into account in order to reduce the complexity of the synthesized antennas and the knowledge of the independently optimum difference excitations, which provide the maximum normalized boresight slope has been exploited. The numerical experiments have pointed out that a proper definition of the sub-array configurations and the corresponding gains allows one to obtain good boresight slope values even though with a limited number of sub-arrays. Constraints on the  $SLL$  have been also taken into account through a hybrid *CPM - CP* approach in order to compare with other state-of-the-art methods dealing with slope maximization.

#### REFERENCES

- [1] S. M. Sherman, *Monopulse Principles and Techniques*. Artech House, 1984.
- [2] G. M. Kirkpatrick, "Aperture illuminations for radar angle-of-arrival measurements," *IRE Trans. Aeronautical Navigational Electronics*, vol. 9, pp. 20-27, Sept. 1953.
- [3] E. T. Bayliss, "Design of monopulse antenna difference patterns with low sidelobes," *Bell System Tech. Journal*, vol. 47, pp. 623-640, 1968.
- [4] D. A. McNamara, "Performance of Zolotarev and modified-Zolotarev difference pattern array distributions," *IEE Proc. Microwave Antennas Propagat.*, vol. 141, no. 1, pp. 37-44, 1994.
- [5] D. A. McNamara, "Synthesis of sub-arrayed monopulse linear arrays through matching of independently optimum sum and difference excitations," *IEE Proc. H Microwaves Antennas Propagat.*, vol. 135, no. 5, pp. 293-296, 1988.
- [6] F. Ares *et al.*, "Optimal compromise among sum and difference patterns through sub-arraying," *Proc. IEEE Antennas Propagat. Symp.*, Baltimore, MD, USA, Jul. 1996, pp. 1142-1145.
- [7] P. Lopez *et al.*, "Subarray weighting for difference patterns of monopulse antennas: joint optimization of subarray configurations and weights," *IEEE Trans. Antennas Propagat.*, vol. 49, no. 11, pp. 1606-1608, 2001.
- [8] S. Caorsi *et al.*, "Optimization of the difference patterns for monopulse antennas by a hybrid real/integer-coded differential evolution method," *IEEE Trans. Antennas Propagat.*, vol. 53, no. 1, pp. 372-376, 2005.
- [9] M. D'Urso *et al.*, "An effective hybrid approach for the optimal synthesis of monopulse antennas," *IEEE Trans. Antennas Propagat.*, vol. 55, no. 4, pp. 1059-1066, 2007.
- [10] L. Manica *et al.*, "An innovative approach based on a tree-searching algorithm for the optimal matching of independently optimum sum and difference excitations," *IEEE Trans. Antennas Propagat.*, vol. 56, no. 1, pp. 58-66, 2008.
- [11] A. Massa *et al.*, "Optimization of the directivity of a monopulse antenna with a subarray weighting by a hybrid differential evolution method," *IEEE Antennas Wireless Propagat. Lett.*, vol. 5, pp. 155-158, 2006.
- [12] P. Rocca *et al.*, "Synthesis of monopulse antennas through iterative contiguous partition method," *Electron. Lett.*, vol. 43, no. 16, pp. 854-856, 2007.
- [13] D. A. McNamara, "Synthesis of sum and difference patterns for two-section monopulse arrays," *IEE Proc. H Microwave Antennas Propagat.*, vol. 135, no. 6, pp. 371-374, Dec. 1988.
- [14] D. A. McNamara, "Maximization of the normalized boresight slope of a difference array of discrete elements," *Electron. Lett.*, vol. 23, no. 21, pp. 1158-1160, Oct. 1987.
- [15] T. T. Taylor, "Design of line-source antennas for narrow beam-width and low side lobes," *Trans. IRE Antennas Propagat.*, vol. AP-3, pp. 16-28, 1955.
- [16] W. D. Fisher, "On grouping for maximum homogeneity," *American Statistical Journal*, 789-798, 1958.
- [17] C. L. Dolph, "A current distribution for broadside arrays which optimizes the relationship between beam width and sidelobe level," *Proc. IRE*, vol. 34, no. 6, pp. 335-348, 1946.
- [18] P. Rocca, L. Manica, and A. Massa, "Hybrid approach for sub-arrayed monopulse antenna synthesis," *Electron. Lett.*, vol. 44, no. 2, pp. 75-76, January 2008.